



Application of thermogravimetric studies for optimization of lithium hexafluorophosphate production

A.A. Smagin *, V.A. Matyukha, V.P. Korobtsev

Siberian Group of Chemical Enterprises Russia, Design and Construction Institute of SGCE, 636070, Seversk, Russia

Accepted 3 March 1997

Abstract

Lithium hexafluorophosphate, isolated from hydrogen fluoride solution (anhydrous) by decanting and filtering, is an adduct of composition LiPF₆*HF. By thermogravimetric investigations the dynamics of HF removal from LiPF₆ by LiPF₆*HF thermal decomposition was studied. Based on the experimental data the constants entering into the equations as $C = C_0^* \exp(t^* K_0^* \exp(-E/RT))$ were calculated, explaining the thermal decomposition processes of LiPF₆*HF and LiPF₆. © 1997 Elsevier Science S.A.

Keywords: Lithium hexafluorophosphate; Thermal decomposition; Thermogravimetric investigations; Reaction rate constant

1. Introduction

Lithium hexafluorophosphate (LiPF₆) is the most promising complex lithium fluoride used essentially as the ionic component of electrolytes for rechargeable chemical cells. The most important figures of merit for this salt, except for the base material content, are the low content of moisture and free acid (in terms of HF). Given increasing demand for LiPF₆ in the world market the design of a high-efficient practice for production of this salt is of prime importance.

In our view, the synthesis method in the following system is of the greatest interest for large-scale production of the salt:

$$LiF + PF_5 \rightarrow LiPF_6$$
 (1)

The selection of this reaction system depends on the scope for using exclusively pure starting components for attainment of the high-quality end product. The Siberian Group of Chemical Enterprises (SGCE) has exclusively developed production practices of pure lithium fluoride with impurity content of less than 0.1 wt.% and spectroscopically pure phosphorus pentafluoride, produced by the efficient process of direct fluorination of elemental phosphorus by gaseous fluorine. Also, the SGCE uses anhydrous hydrogen fluoride (less than 0.03 wt.% of moisture).

The most important steps in the production of high-quality $LiPF_6$ salt in system (1) are pure salt isolation and the removal of residual hydrogen fluoride.

There are two methods for these operations:

- evaporation of HF solution and vacuum drying of the solid residue;
- decanting of HF through a filter, using vacuum or pressure, with subsequent drying of the precipitate.

2. Results

The evaporating of excess hydrogen fluoride was found to cause partial decomposition of the desired product. It appears that the hexafluorophosphoric acid (anhydrous) formed in system (1) on LiPF₆ solvation is subject to decomposition.

$$HPF_6 \xrightarrow{T} HF + PF_5 \tag{2}$$

As a result, the PF₆⁻ ion content in the desired product decreases, and the lithium fluoride content increases appreciably.

The removal of hydrogen fluoride by decantation at temperatures of -80 to $+20^{\circ}$ C resulted in the production of the solid residue constituting free-flowing bulk material including an HF content of 8-11 wt.%.

To study the dynamics of HF removal from the material produced on HF decantation and the optimization of the LiPF₆ production process conditions, thermogravimetric studies were carried out.

Thermogravimetric characteristics were determined for 100-300 mg LiPF₆ samples, produced after HF decantation.

^{*} Corresponding author.

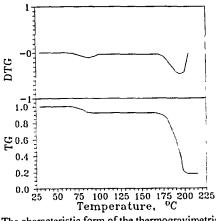


Fig. 1. The characteristic form of the thermogravimetric curves.

The measurements were made in dried nitrogen medium (dew point, -60° C).

The heating rate of the samples was 1-10°C/min.

The characteristic form of the thermogravimetric curves is shown in Fig. 1. The first peak in the DTG curve, observed over the temperature range from 85 to 95°C, defines hydrogen fluoride removal and is due to the thermal decomposition reaction:

$$\begin{array}{c}
\tau \\
\text{LiPF}_6^* \text{HF} \to \text{LiPF}_6 + \text{HF}
\end{array} \tag{3}$$

The second peak in the DTG curve, corresponding to the temperatures $185-195^{\circ}$ C, is due to the thermal decomposition of the base material LiPF₆:

$$LiPF_6 \rightarrow LiF + PF_5 \tag{4}$$

If processes (3) and (4) are assumed to be first-order reactions, then the TG and DTG curves (per unit) may be explained in terms of the concentration of the removed components (HF and PF₅):

$$TG = C_{HF}(T,t) + C_{PFs}(T,t)$$
(5)

$$DTG = d(C_{HF})/dt + d(C_{PFS})/dt$$
 (6)

such that:

$$C_{\rm HF}(T,t) = C_1^* \exp(t^* K_1^* \exp(-E_1/RT)) \tag{7}$$

$$C_{\text{PFs}}(T,t) = C_2^* \exp(t^* K_2^* \exp(-E_2/RT))$$
 (8)

where

- $C_{HF}(T,t)$ (C_1) = HF variable (initial) concentrations;
- $C_{PF_5}(T,t)$ (C_2) = PF₅ variable (initial) concentrations;
- K_1 , K_2 = preexponential in the expression for the rate constant of process (3) and (4), respectively;
- E_1, E_2 = apparent activation energy of HF and PF₅ removal processes, respectively;
- T = temperature, K;
- t = time, min;
- R = 1.987 cal/mol K, gas constant.

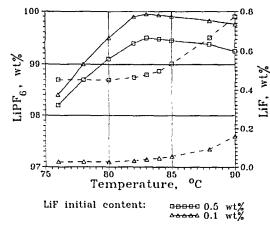


Fig. 2. Base material (———) and LiF (---) impurity content in LiPF₆ against drying temperature of samples with varying LiF initial content.

The coefficients K_1 , K_2 and E_1 , E_2 of functions (7), (8) were calculated by the numerical approximation method for the experimental samples and the following results were derived:

LiPF₆*HF decomposition, process (3), is described by the expression:

$$K(T) = K_1^* \exp(-E_1/RT) \tag{9}$$

where

- $K_1 = (4-5) \times 10^{26}$, min⁻¹;
- $E_1 = 46700 46800$, cal/mol.

 $LiPF_6$ decomposition, process (4), is described by the expression:

$$K(T) = K_2^* \exp(-E_2/RT)$$
 (10)

where

- $K_2 = (1-2) \times 10^7$, min⁻¹;
- $E_2 = 18700 19400$, cal/mol.

The calculated curves of the content in LiPF₆ of the base material and the LiF impurity against the drying temperature at the LiF initial content in the product amounting to 0.1 and 0.5 wt.% are shown in Fig. 2.

The above evaluated constants K_1 , E_1 , K_2 , E_2 of the LiPF₆*HF and LiPF₆ decomposition processes in the starting material were used for the curve calculations.

3. Conclusions

Optimization of the LiPF₆ drying process produces a highquality product with the following characteristics:

- Base material content, wt.% LiPF₆, more than 99.9
- HF, ppm, not more than 100
- LiF, wt.%, not more than 0.08